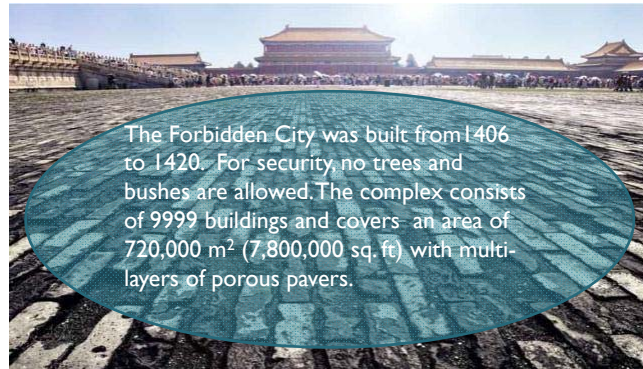
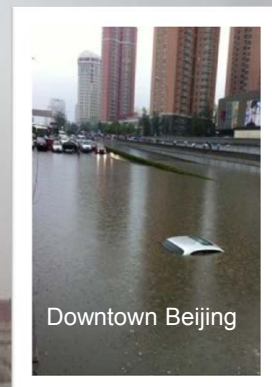


Case Study of LID Designs



James C.Y. Guo, PhD and PE, Professor and Director,
Hydrology and Hydraulics, Civil Engineering,
U. of Colorado Denver

On June 23, 2011, the City of Beijing was severely flooded. The forbidden city was also soaked, but drained well. Why?



GOALS FOR HYDROLOGIC STUDY

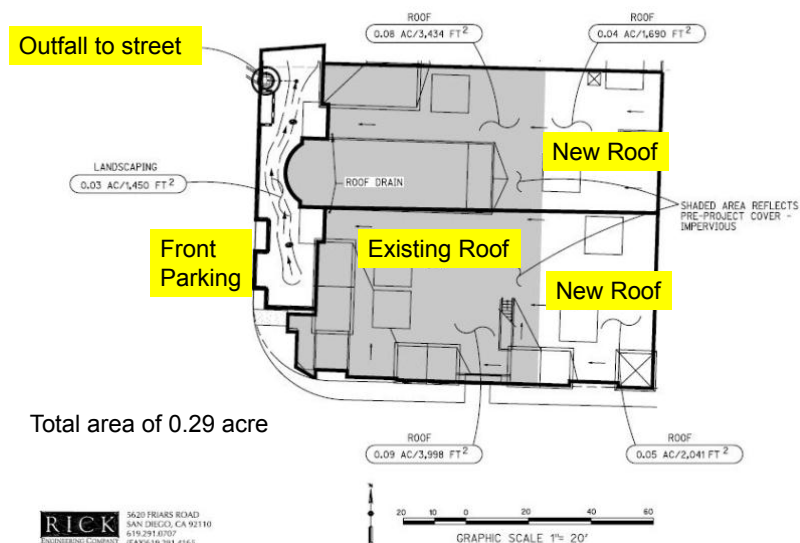
Watershed Flood Mitigation Criteria

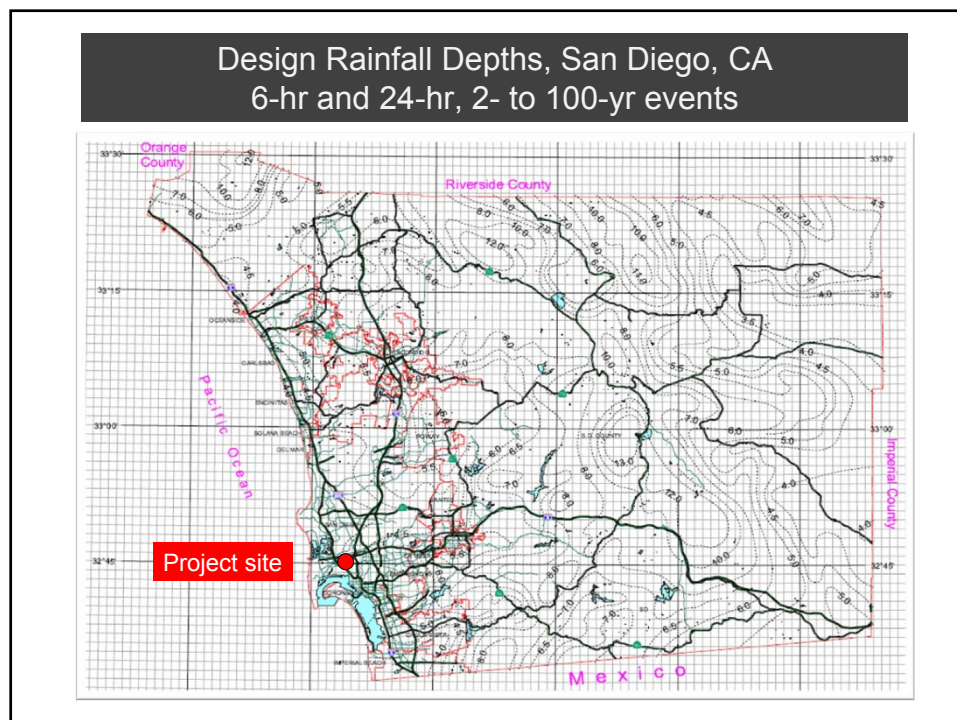
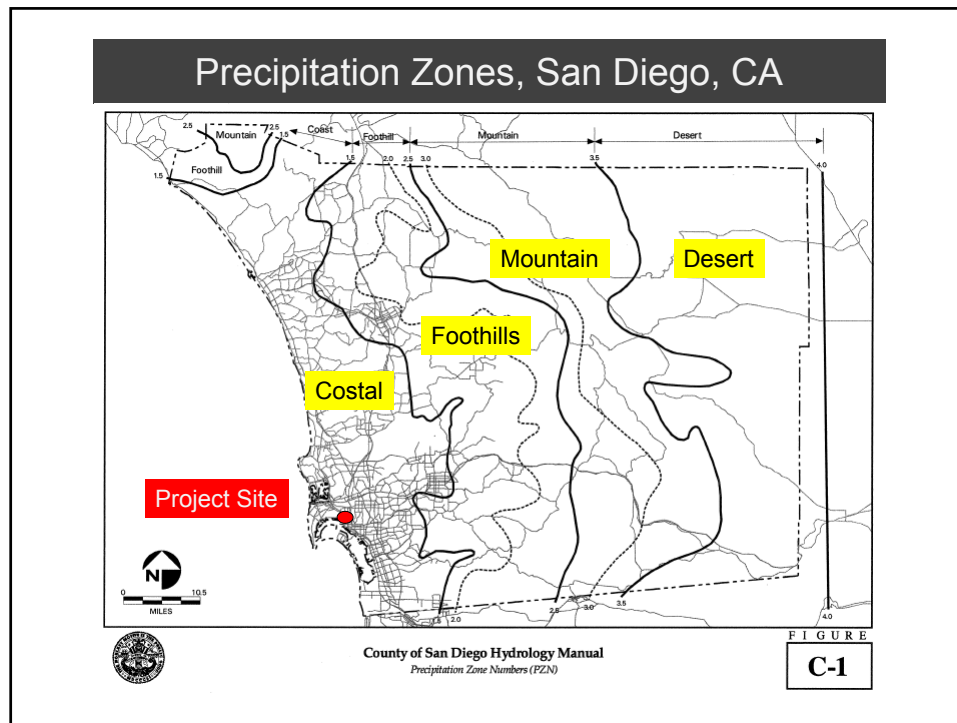
1. Separate storm events within the continuous record
2. Determine extreme events including 85th and 95th rainfall depths
3. Plot flow-frequency relationship
4. Plot flow-duration relationship
5. Model detention mitigation to reduce peak flows
6. Model LID mitigation to reduce runoff volumes
7. Determine the post-project peak flows \leq pre-project peak flows

Watershed Regime Preservation Criteria:

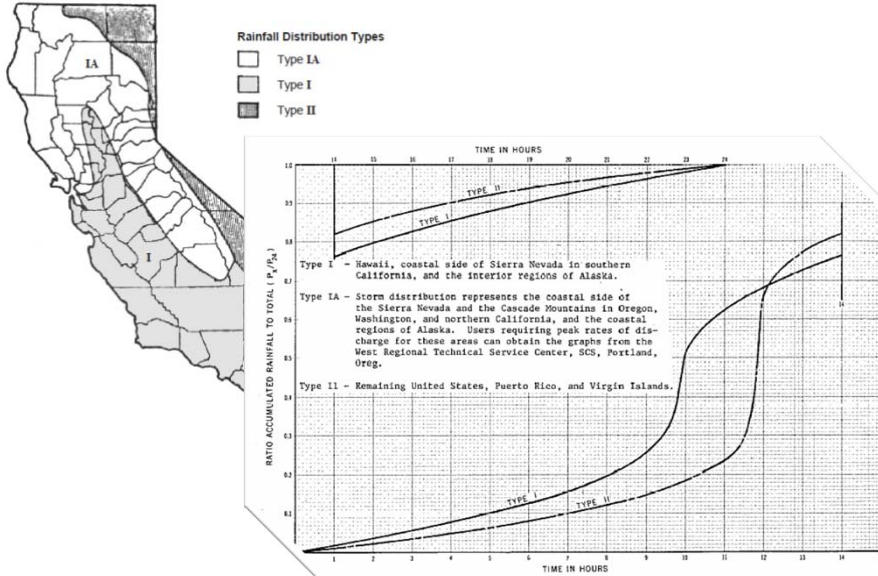
- (1) The post-project flows need to be slightly $<$ the pre-project flows
 - (1-1) for extreme events \geq the 85th storm
 - (1-2) for a range from 0.1Q2 to Q10.
- (2) The post-project total number of hours of flow $<$ the pre-project condition
 - (1-1) between 0.1Q2 and Q10

Stormwater LID Mitigation of New Roof San Diego, CA





Design Rainfall Distribution – SCS 24-hr Type I San Diego, CA



One-hr Continuous Rainfall Record at project site

HOW TO CONVERT SD RAINFALL CONTINUOUS RECORD INTO SWMM INPUT FILE									
Place the cursor below the Yellow Cell to paste the SD Rainfall File									
Month	Day	Year	Hour	P depth	Unit	Gage	SWMM Date	Input for Hour	Rain Depth(in)
Paste below									
10	17	1948	8	0.05 in		CCDA Lindbergh	10/17/1948	8:00	0.05
10	17	1948	9	0.05 in		CCDA Lindbergh	10/17/1948	9:00	0.05
10	17	1948	17	0.01 in		CCDA Lindbergh	10/17/1948	17:00	0.01
10	17	1948	20	0.04 in		CCDA Lindbergh	10/17/1948	20:00	0.04
10	17	1948	22	0.02 in		CCDA Lindbergh	10/17/1948	22:00	0.02
10	17	1948	23	0.02 in		CCDA Lindbergh	10/17/1948	23:00	0.02
10	18	1948	1	0.01 in		CCDA Lindbergh	10/18/1948	1:00	0.01
10	18	1948	2	0.06 in		CCDA Lindbergh	10/18/1948	2:00	0.06
10	18	1948	3	0.11 in		CCDA Lindbergh	10/18/1948	3:00	0.11
10	18	1948	4	0.19 in		CCDA Lindbergh	10/18/1948	4:00	0.19
10	18	1948	5	0.25 in		CCDA Lindbergh	10/18/1948	5:00	0.25
10	18	1948	6	0.12 in		CCDA Lindbergh	10/18/1948	6:00	0.12
10	18	1948	7	0.2 in		CCDA Lindbergh	10/18/1948	7:00	0.2
10	18	1948	8	0.05 in		CCDA Lindbergh	10/18/1948	8:00	0.05
10	18	1948	10	0.01 in		CCDA Lindbergh	10/18/1948	10:00	0.01
10	29	1948	4	0.09 in		CCDA Lindbergh	10/29/1948	4:00	0.09
10	29	1948	5	0.04 in		CCDA Lindbergh	10/29/1948	5:00	0.04
11	3	1948	22	0.03 in		CCDA Lindbergh	11/3/1948	22:00	0.03
11	3	1948	23	0.01 in		CCDA Lindbergh	11/3/1948	23:00	0.01
11	3	1948	24	0.01 in		CCDA Lindbergh	11/3/1948	24:00	0.01
11	4	1948	1	0.01 in		CCDA Lindbergh	11/4/1948	1:00	0.01
11	19	1948	24	0.01 in		CCDA Lindbergh	11/19/1948	24:00	0.01
11	26	1948	11	0.03 in		CCDA Lindbergh	11/26/1948	11:00	0.03

SCS SOIL TYPES A, B, C, and D for selecting hydro losses

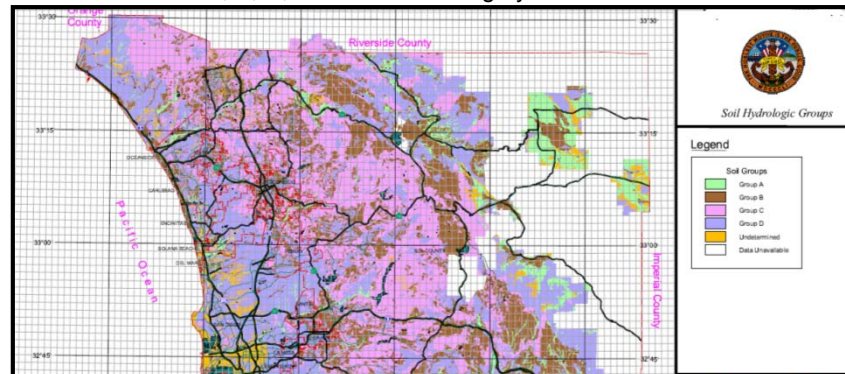


Table 4-4. INFILT Parameters

SCS Hydrologic Soil Group	INFILT Estimate		Runoff Potential
	(in/hr)	(mm/hr)	
A	0.4 - 1.0	10.0 - 25.0	Low
B	0.1 - 0.4	2.5 - 10.0	Moderate
C	0.05 - 0.1	1.25 - 2.5	Moderate to High
D	0.01 - 0.05	0.25 - 1.25	High

Hydrologic Loss: (1) Horton's formula, (2) SCS CN, (3) Green-Ampt

References for City and County of San Diego, CA

Hydromodification Management Plan (HMP) AND **hourly rainfall data for San Diego**. HMP has description of our Peak Flow and Flow Duration performance criteria in Appendix E.

http://www.projectcleanwater.org/index.php?option=com_content&view=article&id=182&Itemid=188

San Diego BMP Sizing Calculator Methodology (Description of San Diego standard bioretention basin and flow-through planter on pages 1-13 and 1-17)

http://www.projectcleanwater.org/images/stories/Docs/LDS/SUSMP/SUSMP_SDB_MP_Sizing_Calculator_Rpt_Jan2012.pdf

San Diego County Standard Urban Storm Water Mitigation Plan (land use "runoff factors" are on page 72 -basically anything impervious has runoff factor=1.0 and most pervious surfaces have runoff factor = 0.1)

<http://www.sdcounty.ca.gov/dpw/watersheds/susmp/susmp.html>

San Diego County Hydrology Manual (if we need this for NRCS runoff parameters or other info)

<http://www.sdcounty.ca.gov/dpw/floodcontrol/hydrologymanual.html>

BASICS: Population of One-hr Precipitation Depths from 1948 to 1977 recorded at San Diego, CA

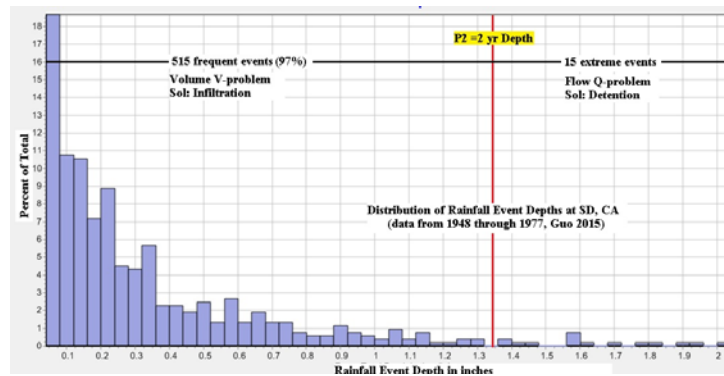
FACTS:

1. Only 15 events out of 30 years >2 yr event (i.e. 3%)
2. 97% of events <2 yr event

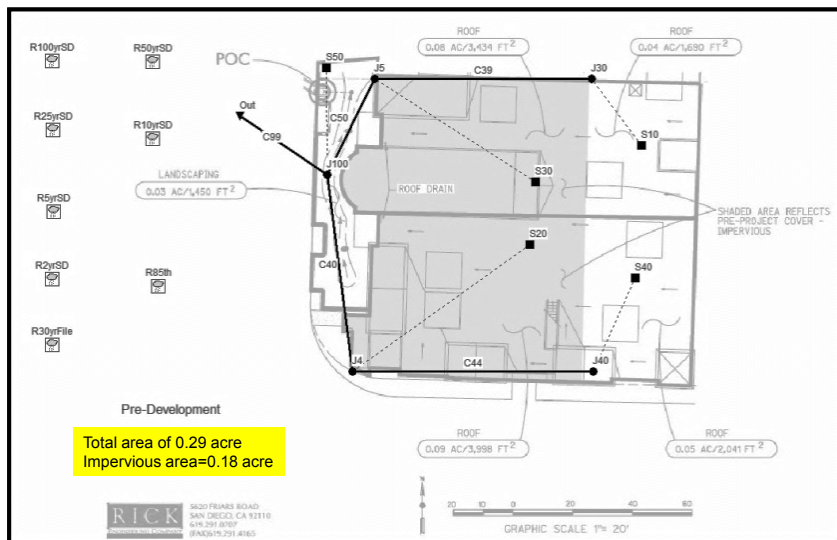
Two stormwater PROBLEMS from urbanization:

Q-problem (peak flow reduction for extreme events)

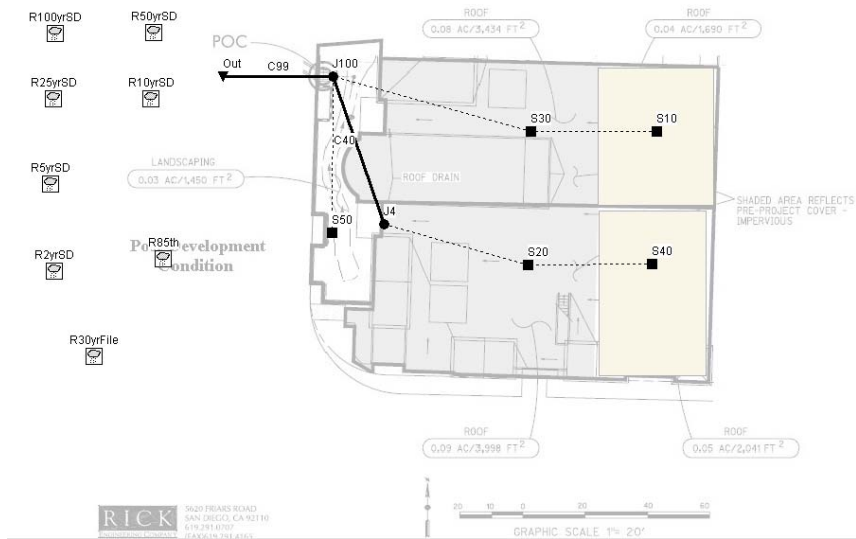
V-problem (runoff volume reduction for frequent events)



SWMM for Pre-development Condition



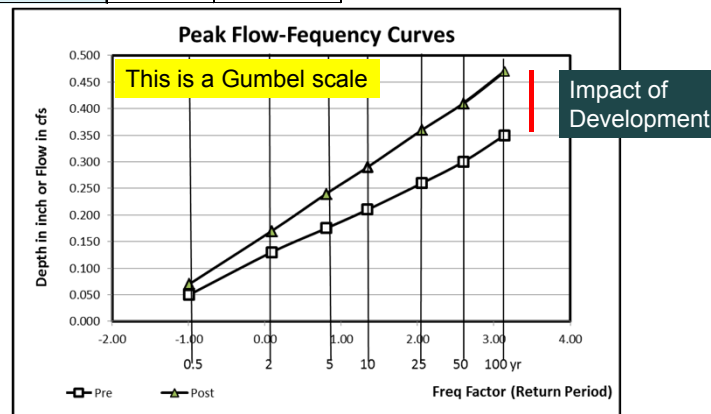
SWMM for Post-development Condition



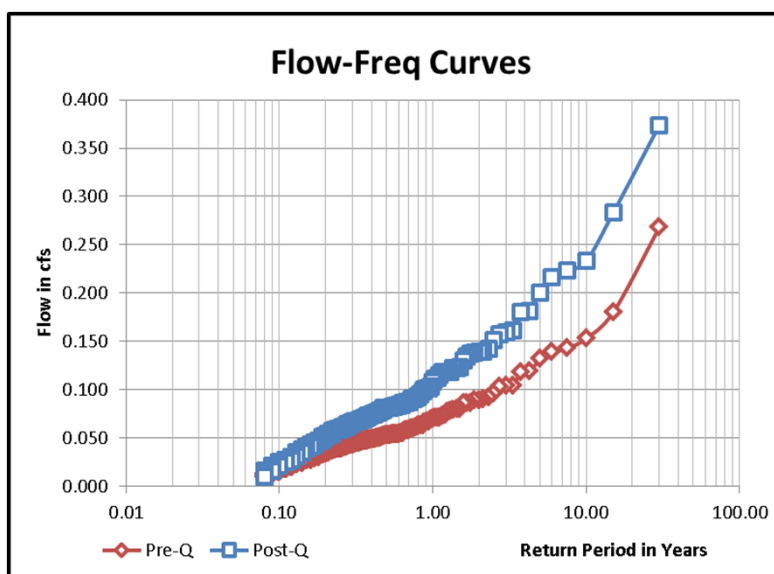
Return Period	P-24 Depth	Pre-Peak Flow	Post-Peak Flow
Tr	P-24	Qp	Qp
year	inch	cfs	cfs
85th or 0.5	0.600	0.050	0.070
2.00	1.500	0.130	0.170
5.00	2.100	0.175	0.240
10.00	2.510	0.210	0.290
25.00	3.100	0.260	0.360
50.00	3.510	0.300	0.410
100.00	4.000	0.350	0.470

Q- Problem
Increase of Peak Flows

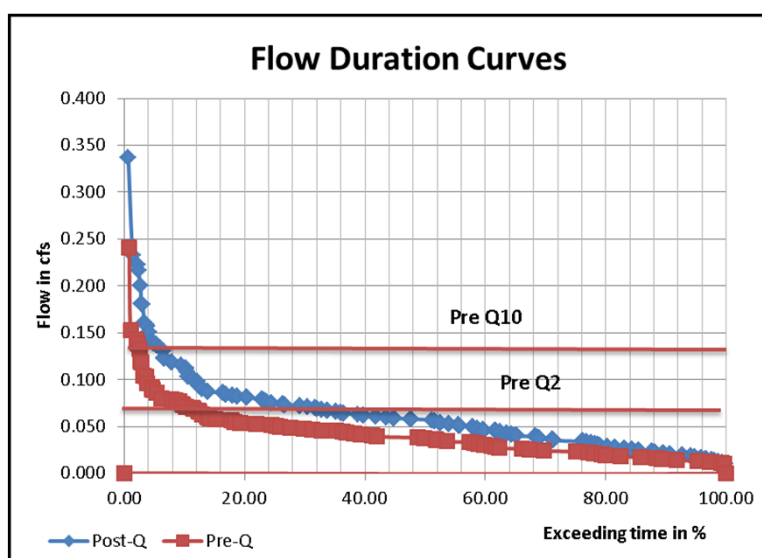
Solution: Flow Detention



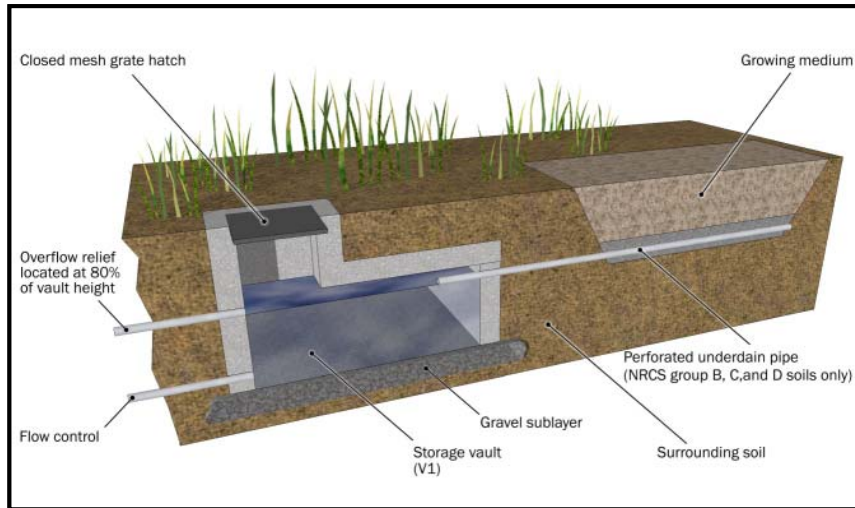
V-Problem = Increase of Runoff Volume (2015)
Solution: Infiltration Facilities such as LID Devices



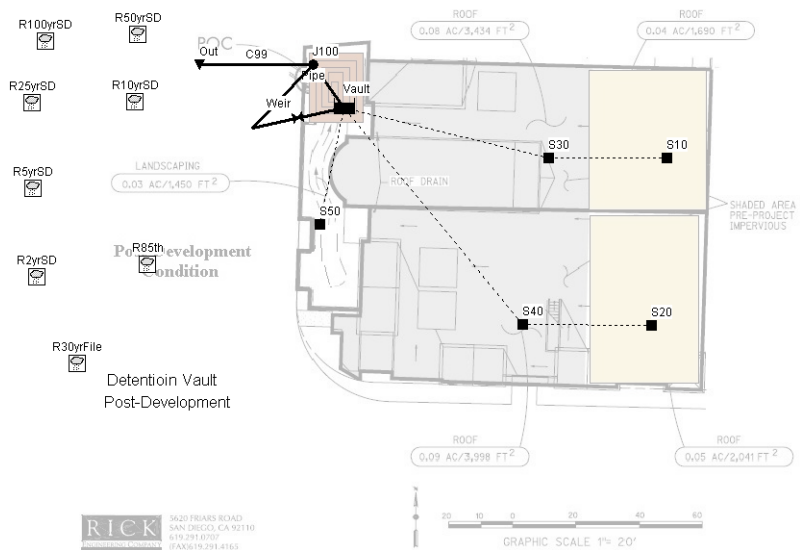
Pre- and Post flow-duration curves at project site (2015)
Problem related to number of events



Underground Detention Vault for Flow Q Reduction



Model with Detention Vault



Flow Detention using Vault --- Flow Q Reduction

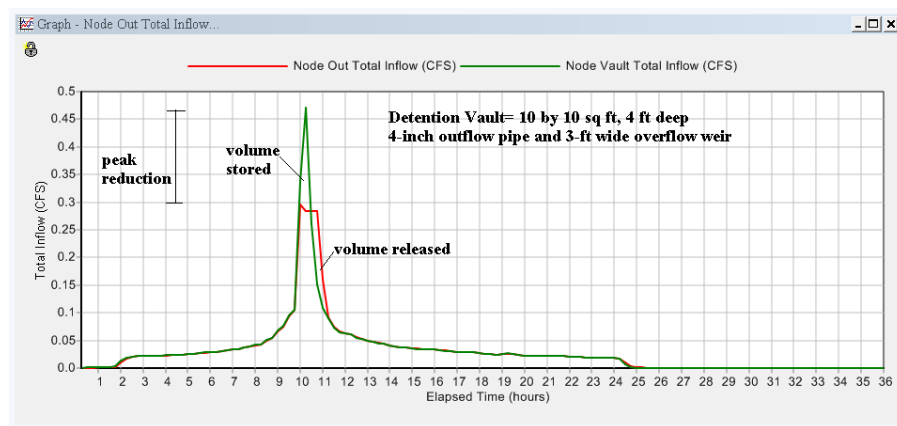
The screenshot shows two windows from a software application. The 'Storage Unit Vault' window on the left displays properties for a vault named 'Vault' at coordinates (2920.133, 7653.910). It lists various parameters such as inflows (NO), treatment (NO), invert elevation (94), maximum depth (4), initial depth (0), ponded area (0), evaporation factor (0), seepage loss (NO), and storage curve (TABULAR). The 'Functional Curve' section shows a coefficient of 1000, an exponent of 0, and a constant of 0. The 'Tabular Curve' section shows the curve name 'MyVault'.

The 'Storage Curve Editor' window on the right shows the 'Retangular Vault' description and a table of depth versus area data. The table has 11 rows, with the first six rows containing data and the remaining five rows empty.

	Depth (ft)	Area (ft2)
1	0	100
2	1	100
3	2	100
4	3	100
5	4	100
6	5	100
7		
8		
9		
10		
11		

Buttons for 'View...', 'Load...', 'Save...', 'OK', 'Cancel', and 'Help' are visible on the right side of the 'Storage Curve Editor' window. A graphic scale of 1" = 20' is shown at the bottom.

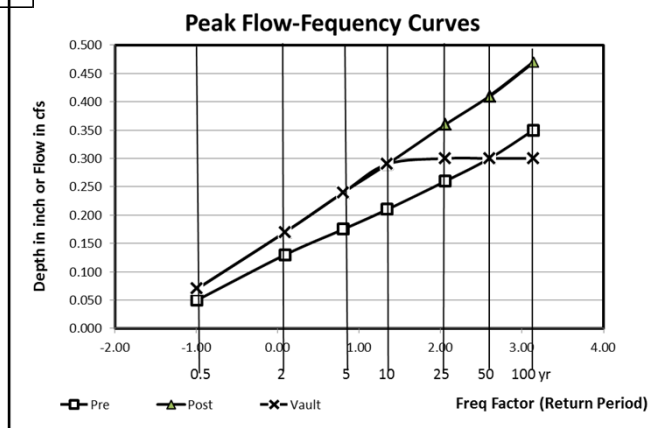
100-yr Peak Flow Reduction thru Detention Vault



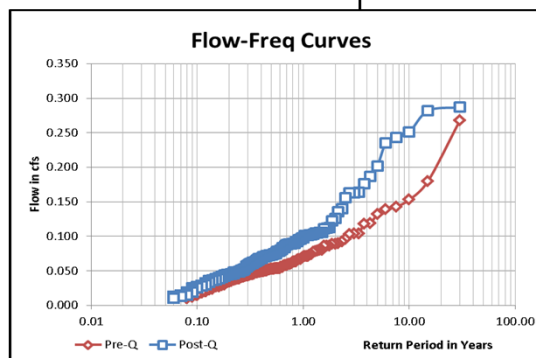
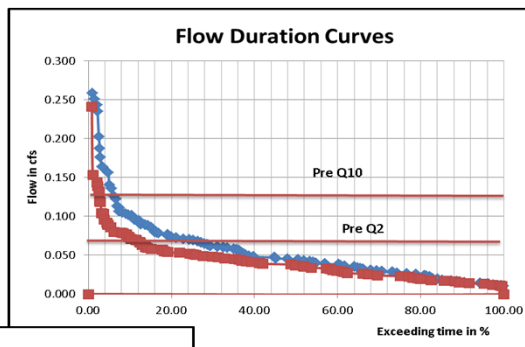
This is an approach to store water and then release it slowly. There is a process to reduce Q, but has NO Volume Reduction at all.

Return Period Tr year	P-24 Depth P-24 inch	Post-Peak Detention Vault cfs
85th or 0.5	0.60	0.07
2.00	1.50	0.17
5.00	2.10	0.24
10.00	2.51	0.29
25.00	3.10	0.3
50.00	3.51	0.3
100.00	4.00	0.3

Effectiveness of Detention Vault
 1. Good Control of Events > Q10
 2. No Control of Events < Q10
 Why?



Underground Vault
 Good Control for the 30-yr Event
 No control for the rest



Discussions on Detention Vault for Q-Reduction

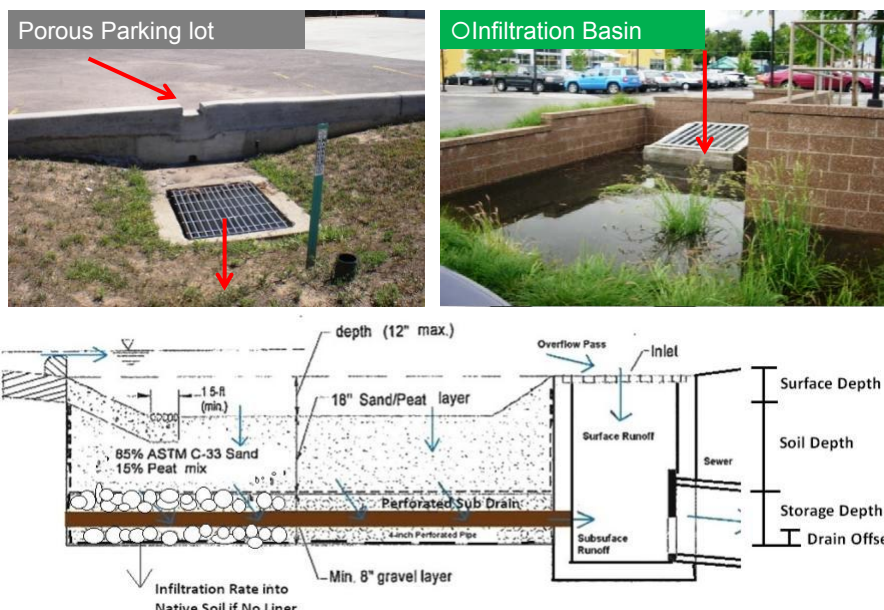
Hydrologic Aspect

1. How to size a vault?
2. Why would the vault only control flows > 10-yr event?
3. How to improve its performance for a full-spectrum peak flow control?
4. If not, how to apply LID designs for a better flow control?
5. What are the major differences in terms of runoff volume treatment between Vault and LID facilities?

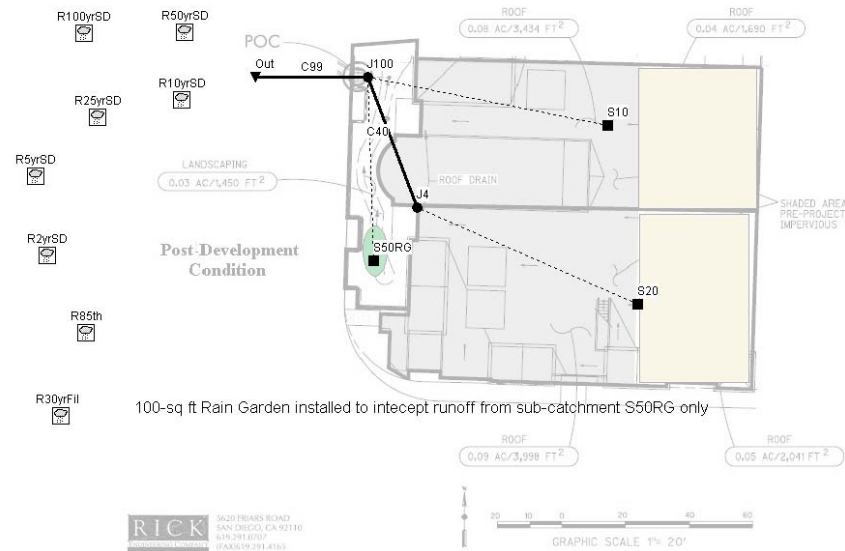
Hydraulic Aspect

1. Considering hydraulic design, what is the major concern when having a vault of 4-ft underground?

Bio Retention Basin



Flow infiltration using a local rain garden – V Reduction



Project | Map

Study Area Map

LID Control Editor

Control Name: Rgarden

LID Type: Bio-Retention Cell

Surface | Soil | Storage | Drain

Berm Height (in. or mm): 10

Vegetation Volume Fraction: 0.1

Surface Roughness (Mannings n): 0.15

Surface Slope (percent): 1.0

Surface | Soil | Storage | Drain

Thickness (in. or mm): 18

Porosity (volume fraction): 0.35

Field Capacity (volume fraction): 0.15

Wilting Point (volume fraction): 0.05

Conductivity (in/hr or mm/hr): 2.5

Conductivity Slope: 10.0

Suction Head (in. or mm): 3.5

Surface | Soil | Storage | Drain

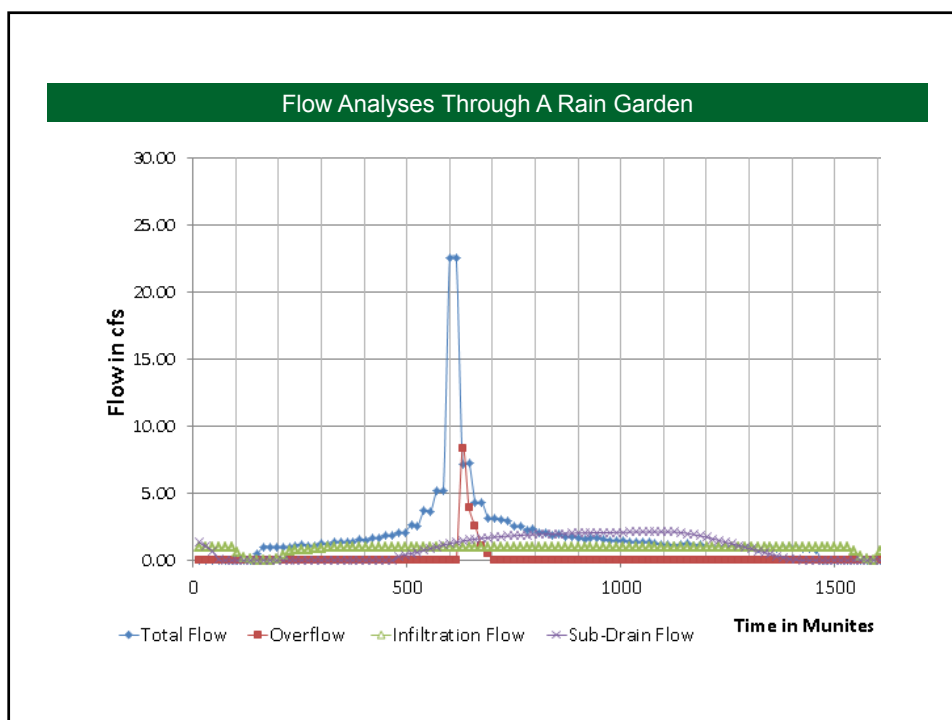
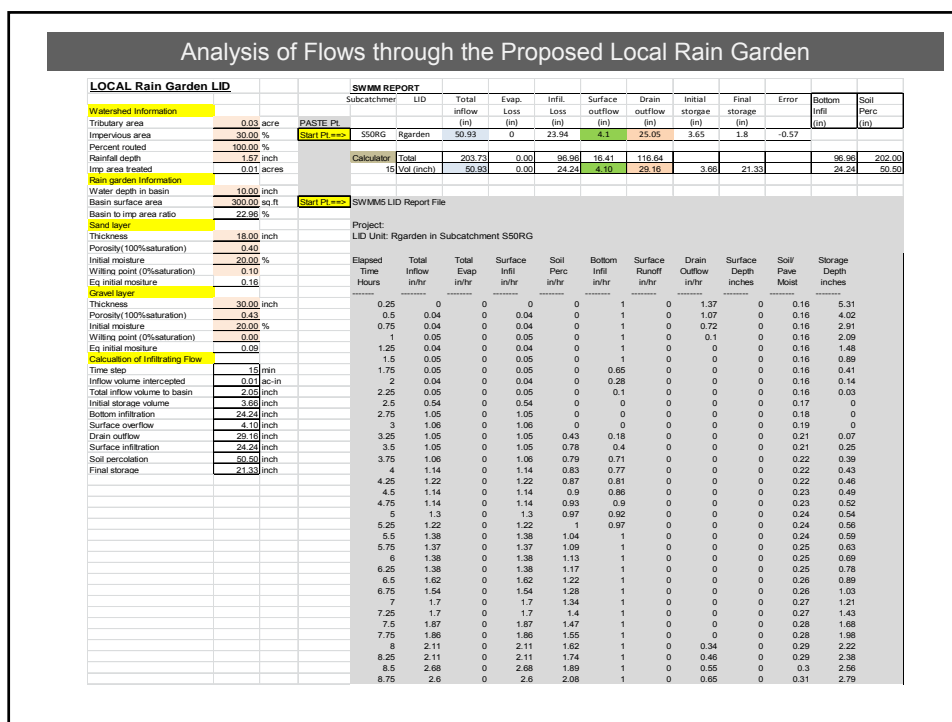
Flow Coefficient*: 0.75

Flow Exponent: 0.5

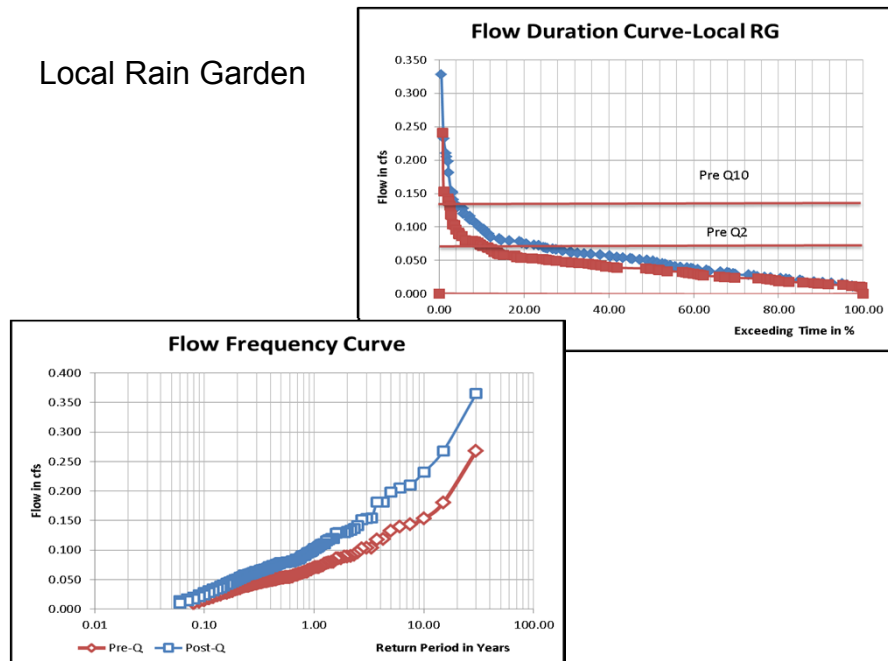
Offset Height (in. or mm): 2

(1) How to create a menu of LID

(2) How to define LID parameters



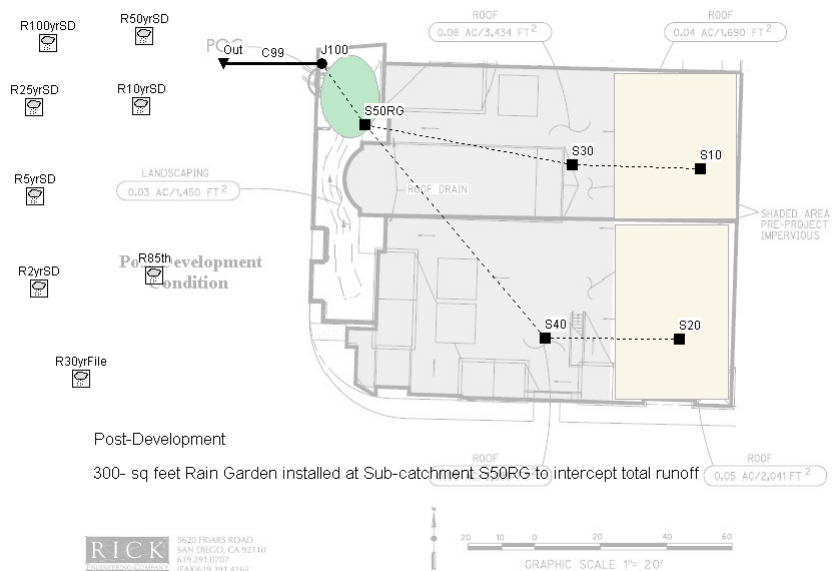
Local Rain Garden



Discussions on LOCAL Rain Garden Design

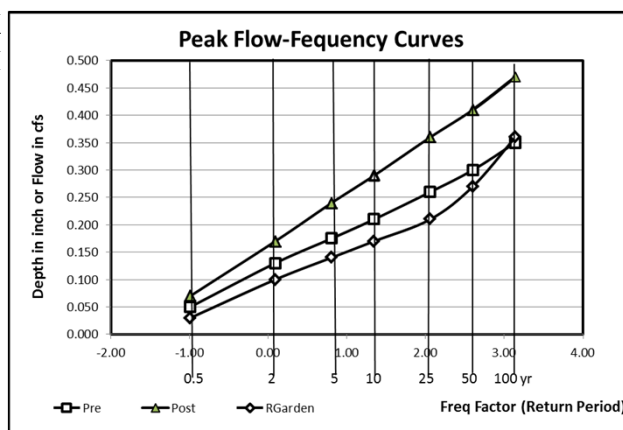
1. How to size a rain garden?
2. Can you revise the model to apply SD's criteria?
3. How to confirm if a rain garden is sufficient?
4. How to convert a local RG into a watershed-wide RG?
5. Pros and Cons between local and watershed-wide RG.
6. How to trace the runoff amount intercepted by the RG?
7. How to trace overtopping flows after the RG became full?
8. Can you tell how the inflow was divided into infiltrating, overtopping, and storage flows through the RG?
9. Define surface infiltrating, mid percolating, and bottom infiltrating flows through a soil column.

300-sq ft Rain Garden for the Entire Watershed

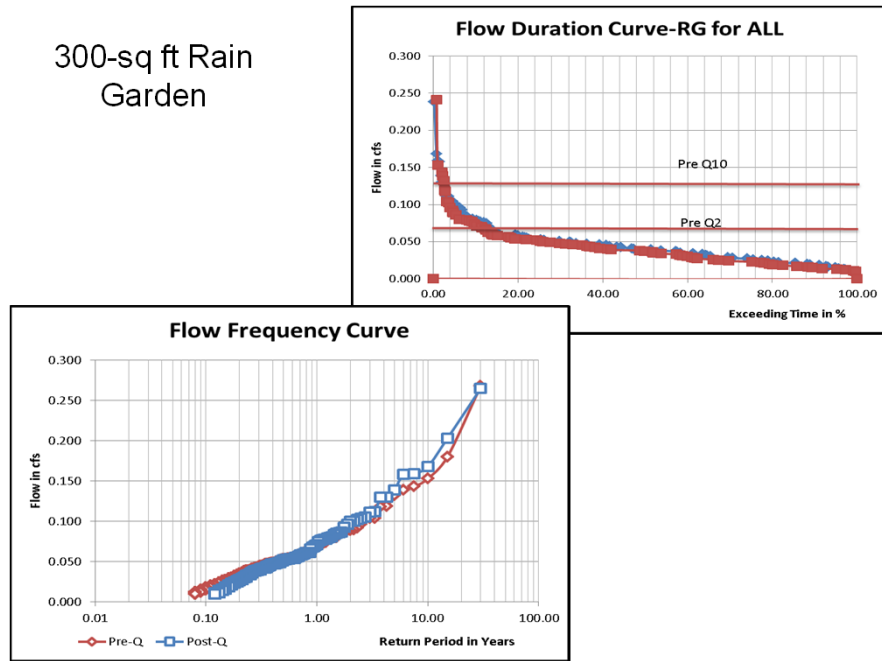


Return Period Tr year	P-24 Depth P-24 inch	Post-Peak Rain Garden cfs
85th or 0.5	0.60	0.03
2.00	1.50	0.1
5.00	2.10	0.14
10.00	2.51	0.17
25.00	3.10	0.21
50.00	3.51	0.27
100.00	4.00	0.36

Effectiveness of 300-sq feet Rain Garden
Not a Good Control for Events < Q10
Good Control for Events > Q50



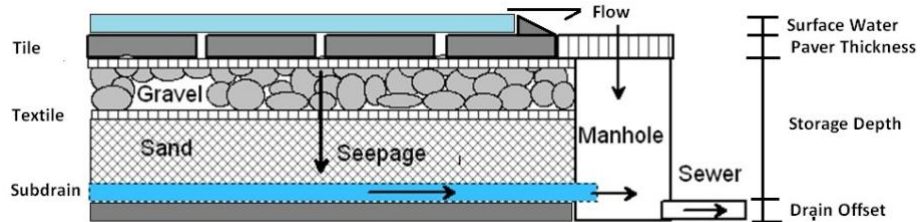
300-sq ft Rain Garden



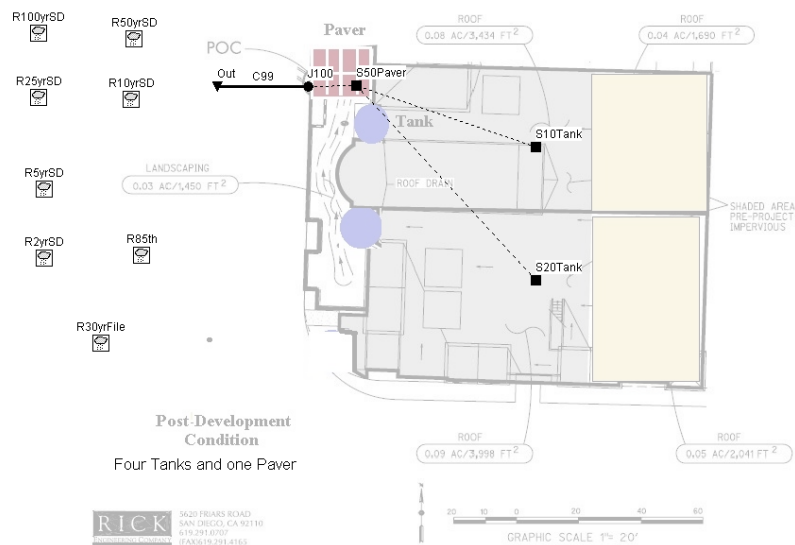
Discussions on Rain Garden Design

1. How to size a watershed-wide rain garden?
2. Can you revise the model to apply SD's criteria?
3. Explain why the infiltrating rate through the filtering medium under the rain garden can be as high as 5.0 in/hr while the infiltrating rate on native soils is reduced to 0.5 inch/hr?
4. Do we need a gravel layer of 30 inches? If so, why?
5. Change the infiltration parameters to see if the rain garden will perform differently? If not, why?
6. How does SWMM treat the deficit of soil antecedent moisture?
7. Shall we also consider unsaturated soil conductivity?
8. What will you do differently if the rain garden is located in a cold zone?

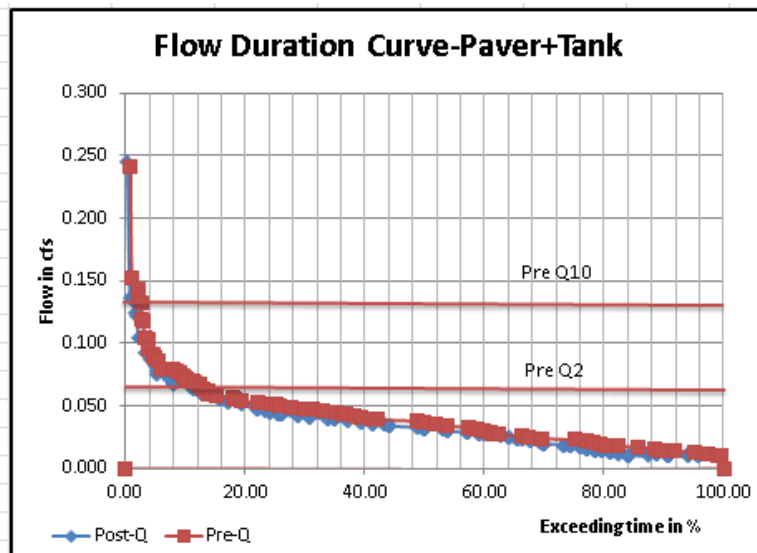
Porous Pavers for Stormwater Disposal --- Source Control



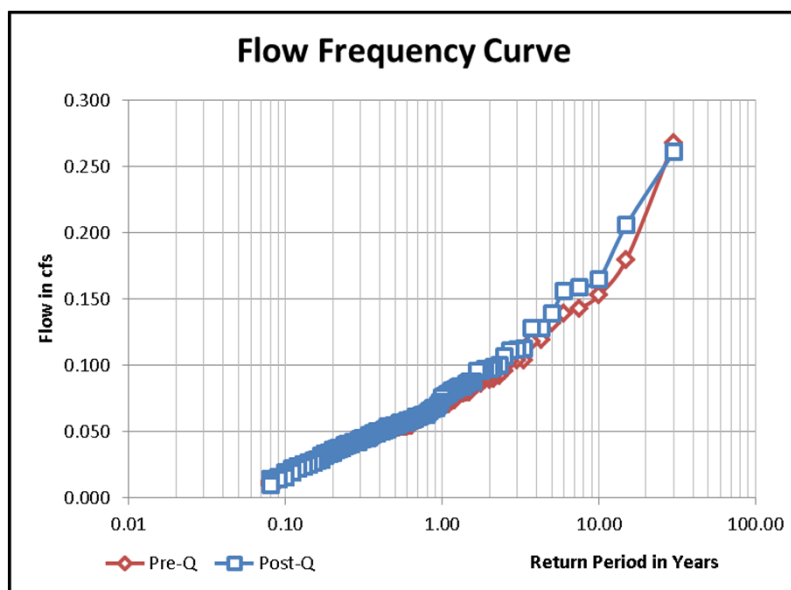
900-sq ft Paver and Rain Tanks



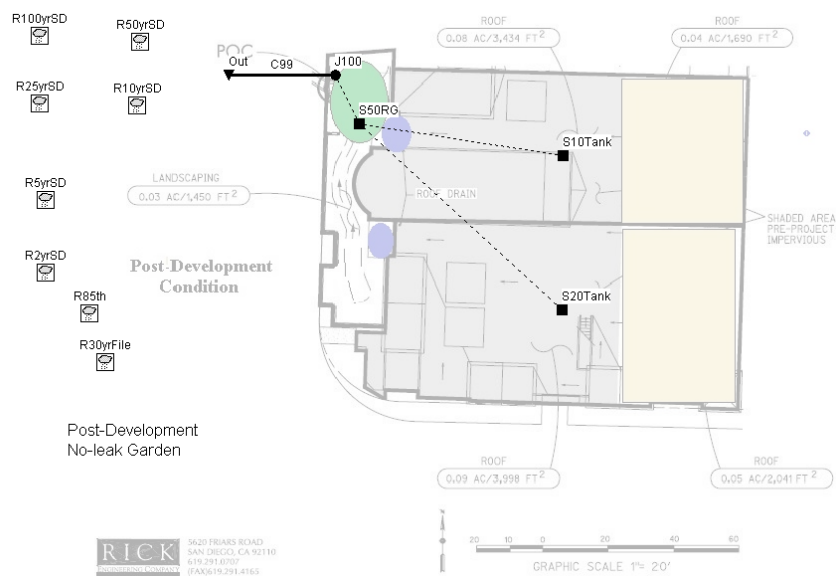
Flow Duration Curves for 900-sq ft Paver and Tanks



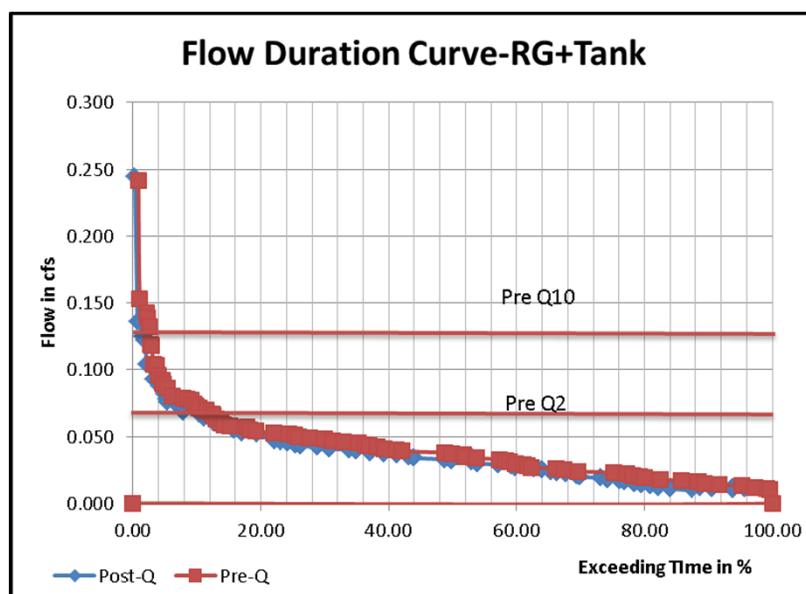
Flow Frequency Curves with 900-sq ft Paver and Tanks



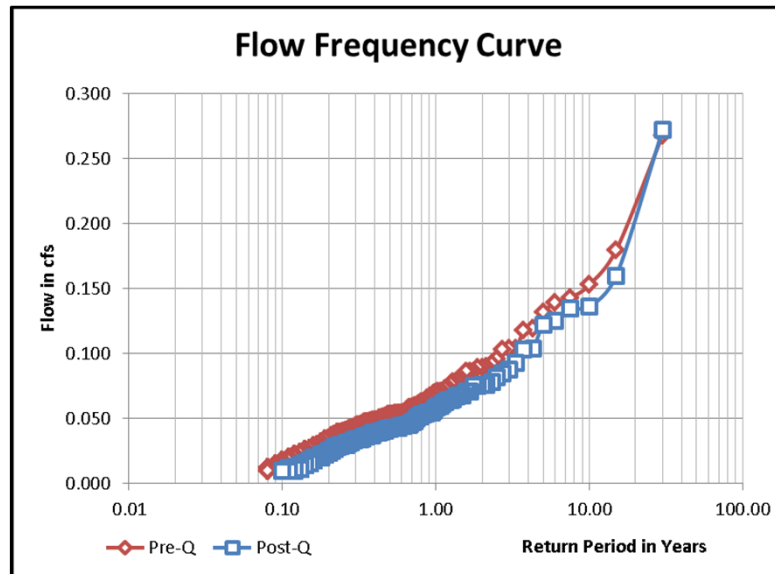
300-sq ft Rain Garden and 2 Tanks



Flow Duration Curves for 300-sq ft Rain Gardens and 2 Tanks



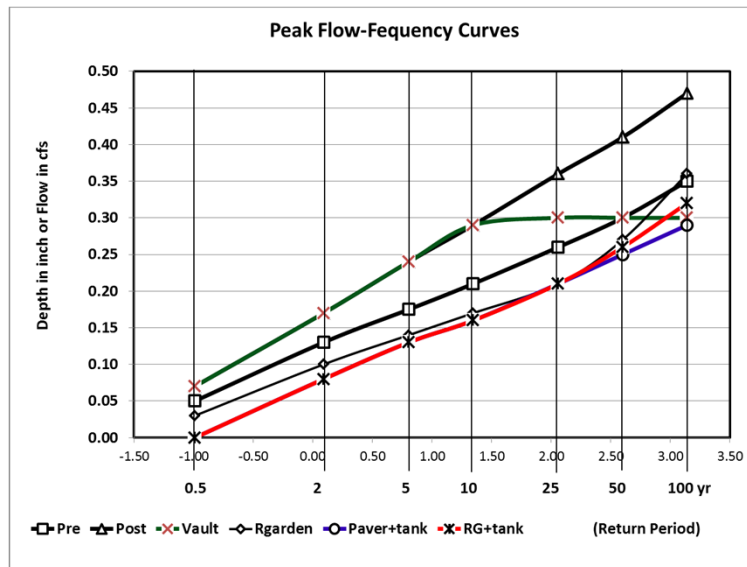
Flow Frequency Curves with 300-sq ft Rain Garden + 2 Tanks



Discussions on Cistern and Bio-Retention Design

1. How to size a rain tank (cistern) according to SD criteria?
2. How to add a cistern to each roof area, i.e. two cisterns for old roof areas, so are for new roof areas.
3. Can you revise the model to have (1) and (2)?
4. Can SWMM model a cistern with a bio-retention for WQ control? If so, how?
5. Exam the effectiveness of these rain tanks for Q2?
6. Show the diminishing effect for Q100.

Flow Frequency Curves with Various Alternatives



Discussions:
How green is green enough?



To get more Info from Dr. James C.Y. Guo

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WWW.UDFCD.ORG

WWW.URBANWATERSHEDS.ORG

- Website
- Free Software
- Training Classes



Porous Pavements in UC-Denver Campus

